

(1-71)  $\sigma_t = \frac{N}{A_{bolt}}$ ,  $18 \times 10^3 \frac{lb}{in^2} = \frac{N}{\frac{\pi}{4} (0.31 in)^2}$   $\rightarrow N = 1,358.6 lb$

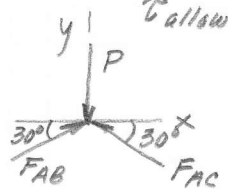
$\sigma_b = \frac{N}{A_{(dia\ washer)} - A_{(dia\ hole)}}$ ,  $2 \times 10^3 \frac{lb}{in^2} = \frac{N}{\frac{\pi}{4} ((0.75 in)^2 - (0.50 in)^2)}$   $\rightarrow N = 490.9 lb$

max allowable tension = **491 lb**

(1-89) F.S. = 2, F.S. =  $\frac{\sigma_{fail}}{\sigma_{allow}} \rightarrow \sigma_{allow} = \frac{6 ksi}{2} = 3 ksi$

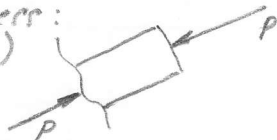
F.S. =  $\frac{\tau_{fail}}{\tau_{allow}} \rightarrow \tau_{allow} = \frac{1.5 ksi}{2} = 0.75 ksi$

joint A:



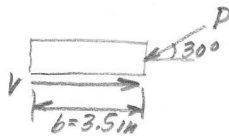
$\sum F_x = 0, F_{AB} = F_{AC}$   
 $\sum F_y = 0, -P + F_{AB} \sin 30^\circ + F_{AC} \sin 30^\circ = 0$   
 $2 F_{AB} \sin 30^\circ = P$   
 $F_{AB} = P$

normal stress:  
(member AB)



$\sigma_{allow} = \frac{N}{A} \rightarrow 3 ksi = \frac{P}{(3 in)(1.25 in)}$ ,  $P = 11.25 kip$

shear stress (at B):



$\tau_{allow} = \frac{V}{A} \rightarrow 0.75 ksi = \frac{P \cos 30^\circ}{(3 in)(3.5 in)}$ ,  $P = 9.09 kip$

(1-91) vertical (gray) member:

max  $\sigma$  (smallest area):  $(\sigma_t)_{allow} = 150 \times 10^6 \frac{N}{m^2} = \frac{P}{(0.006 m)(0.075 m)}$

$P = 67,500 N$  or  $67.5 kN$

bearing of pin (upward):  $(\sigma_b)_{allow} = 220 \times 10^6 \frac{N}{m^2} = \frac{P}{(0.025 m)(0.020 m)}$

$P = 110,000 N$  or  $110 kN$

pin:

double shear:  $(\tau)_{allow} = 130 \times 10^6 \frac{N}{m^2} = \frac{P}{2(0.010 m)(0.025 m)}$

$P = 65,000 N$  or  $65.0 kN$

pin bearing (downward) on horizontal member:

$(\sigma_b)_{allow} = 220 \times 10^6 \frac{N}{m^2} = \frac{P}{(0.005 m)(0.025 m)}$

$P = 55,000 N$  or **55.0 kN**